

5500
User's Manual



© 1996 DH Instruments, Inc. All rights reserved.

Information in this document is subject to change without notice. No part of this document may be reproduced or transmitted in any form or by any means, electronic or mechanical, for any purpose, without the express written permission of **DH Instruments, Inc.** 1905 W. Third St., Tempe, AZ 85281-2490, USA.

DH Instruments and **DH>CalTechnix** make sincere efforts to ensure accuracy and quality of its' published materials; however, no warranty, expressed or implied, is provided. **DH Instruments** and **DH>CalTechnix** disclaim any responsibility or liability for any direct or indirect damages resulting from the use of the information in this manual or products described in it. Mention of any product does not constitute an endorsement by **DH Instruments** and/or **DH>CalTechnix** of that product.

DH>CalTechnix, **DH Instruments**, **DH** and **DHI** are registered trademarks.

Document No. 550006
861000
Printed in the USA.



TABLE OF CONTENTS (cont.)**CHAPTER 5 - MAINTENANCE**

5.1	Changing the Mounting Post O-Ring Assembly	35
5.2	Changing the Quick-Connecting Head O-Ring Assembly	36
5.3	Replacing the Drive Belt	37

CHAPTER 6 - TROUBLESHOOTING

	Troubleshooting	38
--	-----------------	----

CHAPTER 7 - SCHEMATIC

	Hydraulic Circuit Schematic	40
--	-----------------------------	----

ANNEXES

	Annexes	41
--	---------	----



TABLE OF CONTENTS

CHAPTER 1 - INTRODUCTION

1.1	Purpose	1
1.2	Operating Principle	1

CHAPTER 2 - DESCRIPTION

2.1	Component Check List	2
2.2	Component Location with Manufacturer's Reference Numbers	3
2.3	Description of the Components	4

CHAPTER 3 - INSTALLATION AND START-UP

3.1	The Standard as Delivered	14
3.2	Installing the Piston-Cylinder	14
	Cleaning the Piston-Cylinder	14
	Removing the Piston-Cylinder Plug	15
	Installing the Piston-Cylinder	16
	Filling the Lubrication Circuit	17
	Purging the Lubrication Circuit	18
	Purging the Standard	19
	Removing the Piston-Cylinder	19
3.3	Start-Up	20
3.4	Calibrations: Elevated Static Pressure	20
3.5	Calibrations: Static Pressure	21
3.6	Particularities of Pneumatic Operation	21
3.7	Precautions to be Taken To Assure Good Measurements	22
3.8	Shut-Down Procedure	22
3.9	Periodic Maintenance	22
3.10	Periodic Operational Check	23
3.11	Recalibration of Piston-Cylinder and Masses	23
3.12	Moving the Standard	23
3.13	Shipping the Standard	24
3.14	Storing the Standard	24

CHAPTER 4 - METROLOGICAL THEORY OF THE PRESSURE STANDARD

4.1	Fundamental Theory	25
	Correction for Acceleration Due to Gravity	26
	Correction of Effective Area as a Function of Temperature	27
	General Formula	27
	Air Head Correction	27
4.2	Pressure Calculation	29
	Calculation of the Local Conversion Coefficient at 20°C	29
	Calculation of the Pressure at the Reference Level of the Standard	29
	Calculation of the Pressure at the Height of the Instrument Under Test	29
4.3	Accuracy of the Pressure Standards	29
4.4	Temperature Probe (S', S and S ² accuracy only)	31
	Measuring Principal Measurements	31
	Measurements	31



CHAPTER 1 - INTRODUCTION

1.1 PURPOSE

DHI Model 5500 Pressure Standards are pneumatically operated deadweight testers used to calibrate and test gauges, transducers and transmitters at pressures up to 4 000 psi with a 5501 and 8 000 psi with a 5502. NOTE: 16 000 psi available on special order.

1.2 OPERATING PRINCIPLE

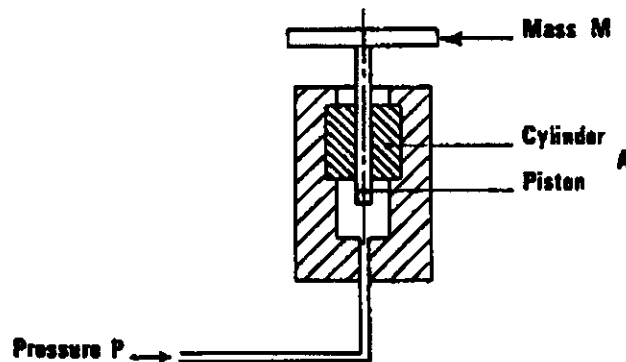
The key component is the mounting post which combines the primary metrological elements:

- 1) The piston-cylinder which defines an effective area, A.
- 2) The masses, of global value M, which act upon the piston.

The value of the pressure, P, which puts the piston into equilibrium is given by the formula:

$$P = \frac{Mg}{A}$$

g = Acceleration due to gravity



Operating Principal



(User Notes)

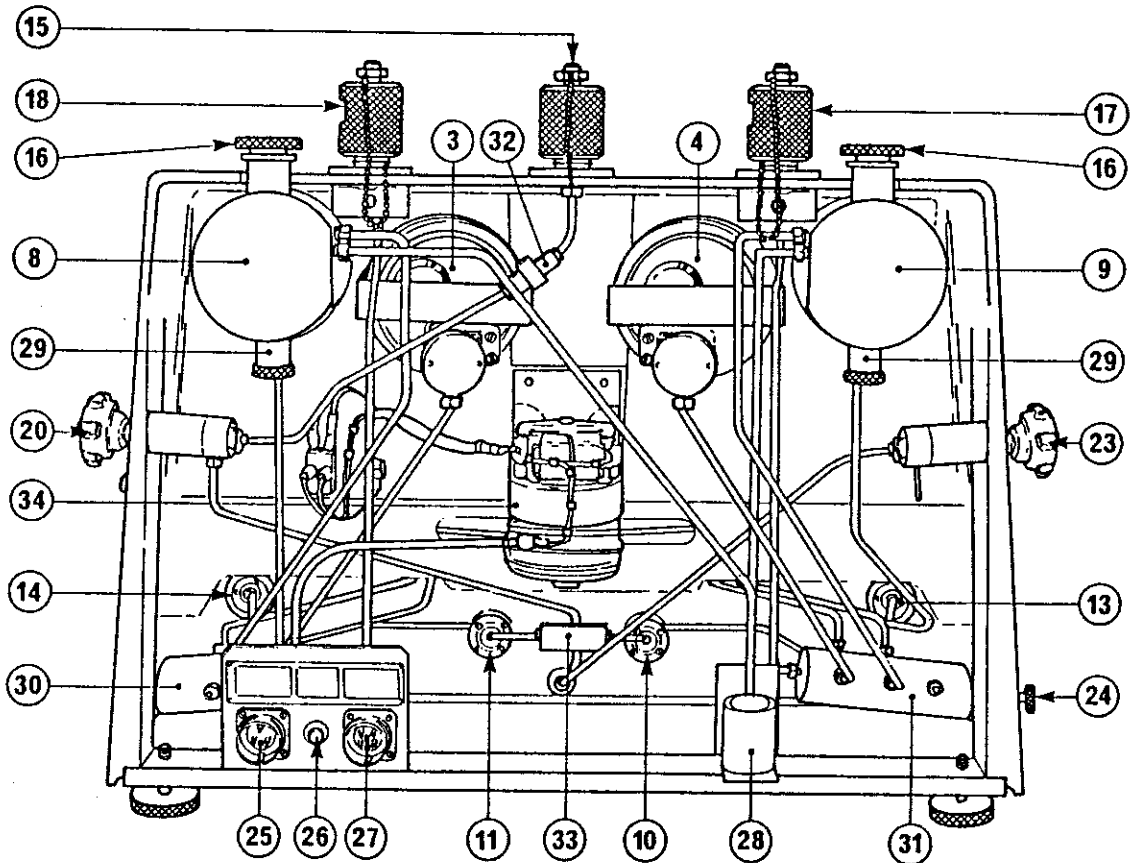
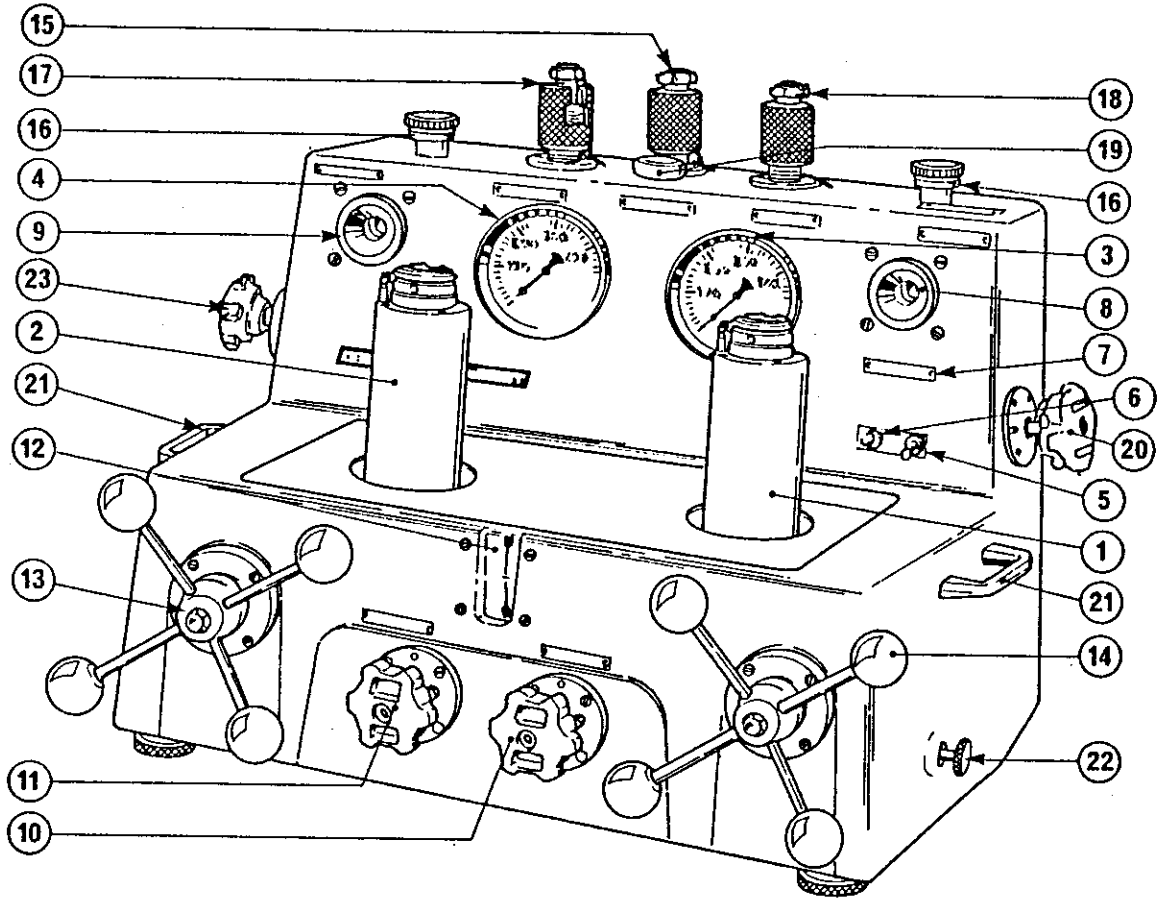


CHAPTER 2 - DESCRIPTION

2.1 COMPONENT CHECK LIST

- **Housing** : Light alloy casting, housing all the components necessary for operation. Delivered in a wooden cabinet.
- **Mass Set** : Total value is generally 40 kg (x2). The masses are supplied in a series of wooden storage cases.
- **Piston-Cylinder** : Supplied in a carrying case with a special mounting tool.
- **Standard Accessories**
 - User's Manual
 - Calibration Certificate with Technical Data
 - Litre Spinell
 - Drive Belt, p/n- 665
 - 2 @ Piston Travel Limit Pins, p/n- 30199
 - 4 @ Adjustable Feet, p/n- 37613
 - Plastic Cover, p/n- 31114
 - O-Ring Assembly Mounting Tool, p/n- 40957
 - Circlip Special Tool, p/n- 37351
 - 4 @ O-Rings, p/n- R13 PC 851
 - O-Ring Assembly for the Quick Connecting Head, p/n- 41087
 - DH 1500 Gland Nut
 - DH 1500 Plug
 - 3 @ DH 1500 Pressure Fittings
 - 2 @ Mass Carrying Bells
 - Oil Run-Off Cup, p/n- 39509
 - 250 mA Delayed Fuse
 - Power Supply Cable
 - RTD Output Cable (S accuracy only)





2.2 COMPONENT LOCATION WITH MANUFACTURER'S REFERENCE NUMBERS

The Model 5500 is made up of a rigid housing into which the following components are integrated:

- **Center**
 - 1) The mounting post into which the piston-cylinder is installed, p/n- 41074 (p/n- 41531 for S class)
 - 2) Comparison post, p/n- 41074

- **Upper Front Face**
 - 3) Pressure gauge, p/n- 232
 - 4) Pressure gauge, p/n- 232
 - 5) Power ON/OFF switch, p/n- 527
 - 6) ON/OFF indicator light, p/n- 380627-2
 - 7) Piston reference level line
 - 8) Measuring element visible level lubricant reservoir, p/n- 41076
 - 9) Comparison element visible level lubricant reservoir

- **Lower Front Face**
 - 10) High pressure isolation valve, p/n- 40912
 - 11) Low pressure isolation valve, p/n- 40912
 - 12) Piston displacement indicator, p/n- 30286
 - 13) Variable volume screw press, p/n- 41506
 - 14) Variable volume screw press, p/n- 41506

- **Top**
 - 15) Gas supply connection, p/n- 41951
 - 16) Lubricant reservoir plug
 - 17) Low pressure connection, p/n- 41951
 - 18) High pressure connection, p/n- 41951
 - 19) Bubble level

- **Right Side**
 - 20) Gas inlet valve, p/n- 40912
 - 21) Carrying handle
 - 22) Drain valve

- **Left Side**
 - 23) Gas exhaust valve, p/n- 40912
 - 21) Carrying handle
 - 24) Drain cock

- **Rear**
 - 25) Main power connection
 - 26) Fuse, p/n- 19201
 - 27) Temperature probe connection (S Class only)
 - 28) Waste oil run-off cup



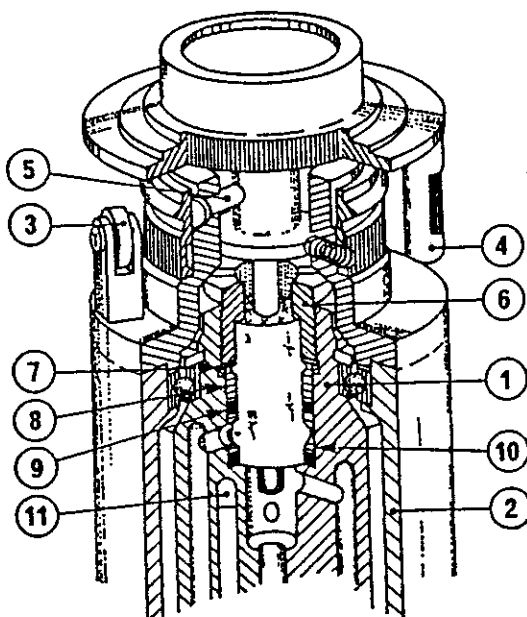
- **Inside**

- 10, 11, 20 & 23) Valves
 - 13 & 14) Variable volume screw press
 - 8) Visible level reservoirs with drain cock (29)
 - 30 & 31) Pressure manifold, p/n- 40888
 - 3 & 4) Pressure gauges
 - 32 & 33) Gas line filters, p/n- 41060
 - 34) Drive motor, p/n- 40454 (220/240 v)
- Interconnecting pipework

The housing is closed in the rear by a steel panel held by a quick disconnect pin.

2.3 DESCRIPTION OF THE COMPONENTS

- **Mounting Post**



Function: Piston-cylinder mounting post

Description: Stainless steel body (1) over which a pulley (2) is mounted on bearings. The pulley is rotated by the motor using a drive belt. The pulley assures piston rotation using the drive pin (3) which occasionally pushes the pin (4) on the piston plate.

- 5) Piston travel limit pin
- 6) Cylinder retaining nut
- 7) Circlip
- 8) Spacer
- 9) O-Ring
- 10) Spacer
- 11) Platinum RTD (S Class only)

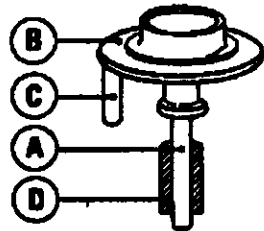
- **Comparison Mounting Post**

Function: Same as above.

Description: Same as above. Both the measuring element and the comparison element are supplied in a wooden storage case.



- **Piston-Cylinder**



Function: Fundamental metrological element which transforms the pressure into a measurable proportional force.

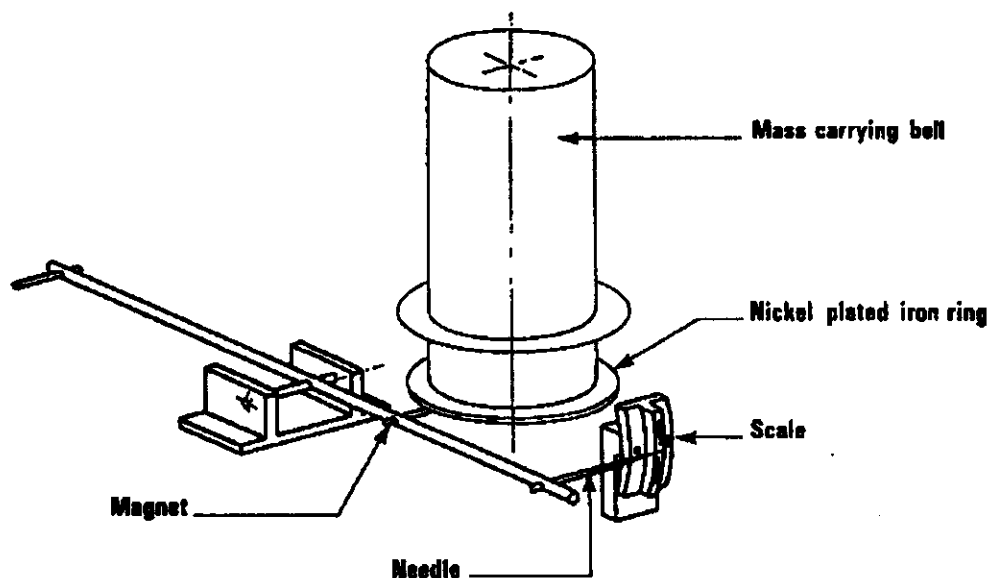
Description: The piston (A) is equipped with a plate (B) on which is mounted a pin (C). The cylinder (D) is always made of tungsten carbide and the piston is made of tungsten carbide or steel.

Piston-cylinders of different effective areas are interchangeable. All pistons have the same mass (0.2 kg) and all cylinders have the same external dimensions.

- **Piston Displacement Indicator**

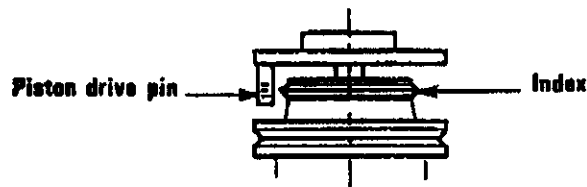
Function: To give a precise indication of piston position and of its movement.

Description: It is a lever that moves in the same direction as the piston. On the lever is a needle which is visible on a scale on the front of the standard. The scale indicates upper and lower end of stroke position as well as the mid-stroke equilibrium point. The lever moves via a magnet which tracks a nickel plated iron ring on the mass carrying bell without interfering with its movement. The indication given by the needle is a 4X amplification of actual piston movement.

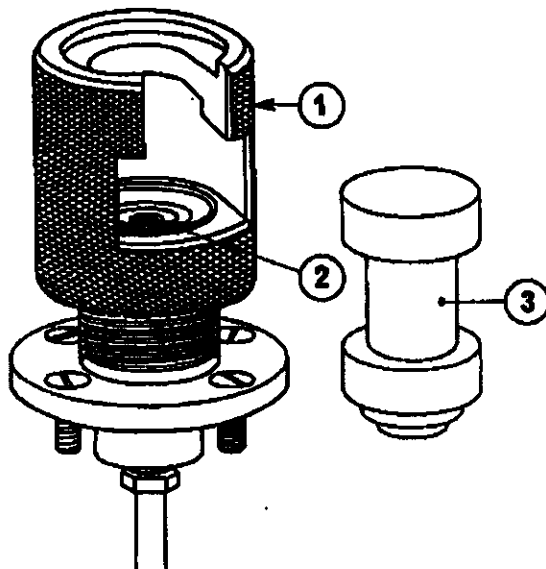


- **Piston Displacement Indicator** continued

NOTE: When working without the mass carrying bell, the mid-stroke equilibrium point is identified by the middle marking on the piston drive pin when it is in line with the index ring.



- **Quick-Connecting Head**



Function: Connection point to the system under test.

Description: A convenient connection which will not be damaged or wear despite many make and break operations. The knurled nut (1) tightens onto a connector (3). An O-ring assembly (2) makes the seal. The knurled nut is tightened by hand even at the highest pressures. The quick connecting head is an interchangeable sub-assembly but general maintenance requires only the replacement of the O-ring assembly.

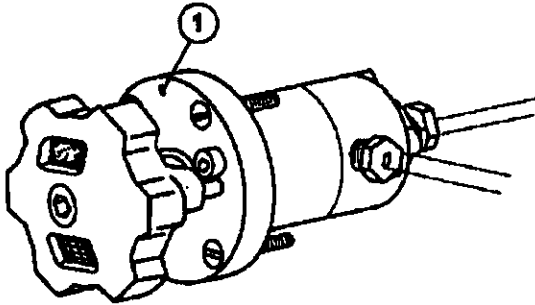
NOTE: Many different pressure connectors for the quick-connecting head are available.



- **Valve**

Function: To isolate one part of the hydraulic circuit from another.

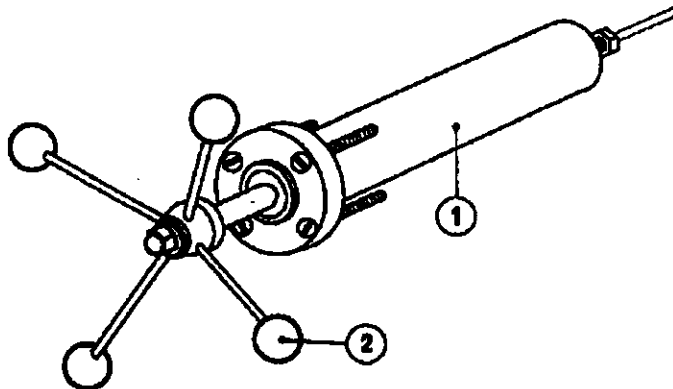
Description: In the closed position, the red label on the handle is across from the white reference dot (1). A Belleville spring pushes the needle onto its seat. The handle feels loose when valve is closed. The opening of the valve is progressive and made by turning the handle clockwise to compress the spring. Rotation of the handle is limited to a half turn by stops. The valve is an interchangeable subassembly.



- **Variable Volume Screw Press**

Function: Pressure generation and regulation up to 20,000 psi.

Description: A cylinder (1) in which a plunger moves by turning a handle (2). Variation of volume for the entire plunger stroke is 15 cm³. Variations for one handle turn is 0.35 cm³.



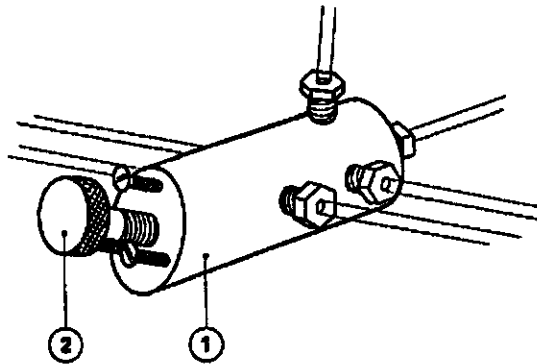
The variable volume screw press is an interchangeable sub-assembly.



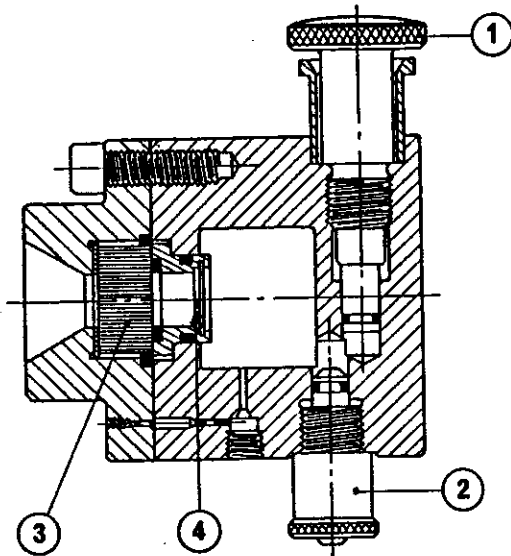
- **Sump**

Function: Located at the low point of the internal circuitry to serve as a purge point. Serves as manifold for internal tubing.

Description: A cylinder (1) with the fittings needed for the connection of internal tubing. A drain-cock (2) allows system purge. The sump is an interchangeable sub-assembly.



• **Visible Level Reservoir**



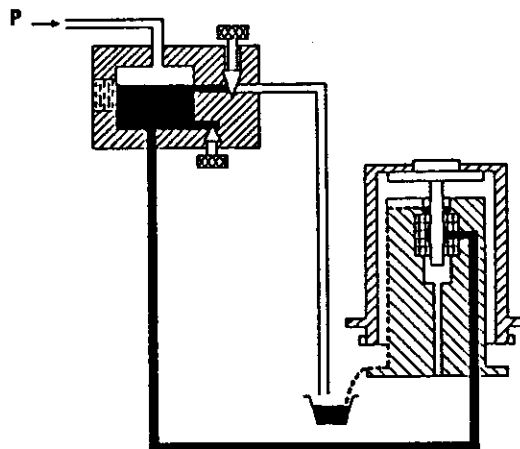
Function: Hold piston-cylinder lubricating fluid.

Description: A cylindrical vessel designed to withstand maximum system pressure. A cap (1) on the top closes the fill opening. A purge screw (2) on the bottom empties the vessel. The front face is a synthetic sapphire (3) which allows visual determination of fill level. The pointer shows a good average fill level. Three lateral connections allow:

- outward flow of lubricant towards the piston-cylinder
- inflow of pneumatic pressure
- fluid overflow in the case of overfill

The visible level reservoir is an interchangeable sub-assembly.

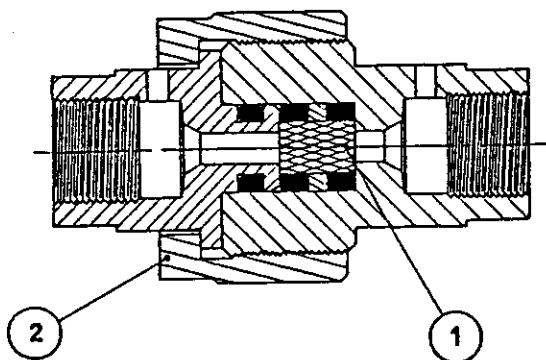
Piston-Cylinder Lubrication Principle



- **Filter**

Function: Protect the system from contaminants in the pressure medium.

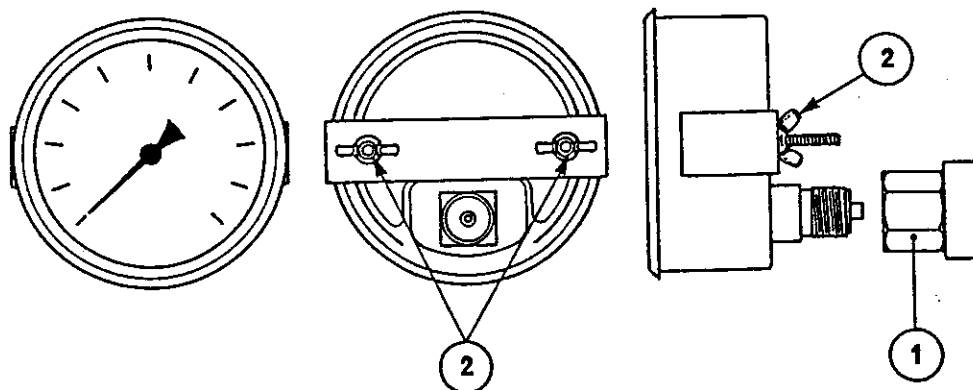
Description: A woven metal mat (1) collects impurities. The nut (2) allows the filter to be opened and cleaned.



- **Indicating Gauge**

Function: Give an immediate visual indications of approximate pressure in the system.

Description: Bourdon tube gauge. The gauge is an interchangeable sub-assembly.

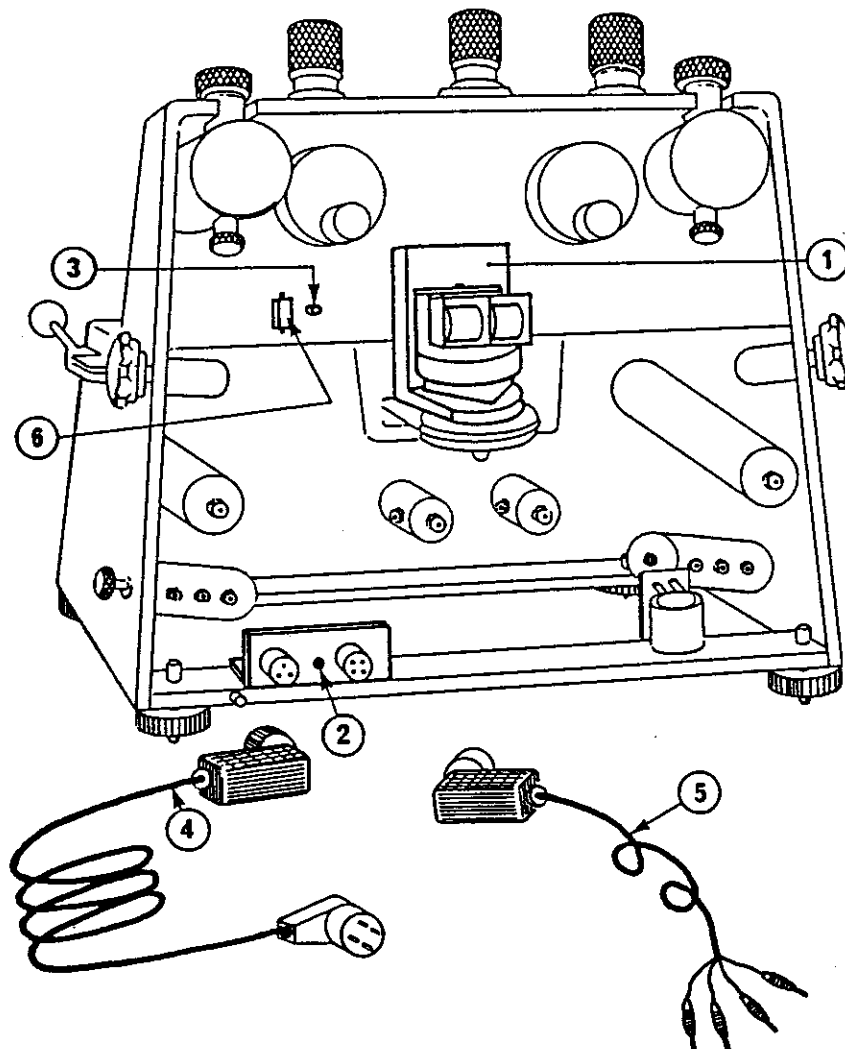


- **Electrical System**

- A) **Motor**

Function: For piston rotation using a drive belt and the mounting post pulley.

Description: Made up of a 30 rpm squirrel cage motor (1), an ON/OFF switch (6), an ON/OFF indicator light (3), a fuse (2), a 2.5 meter power supply cable (4) and the RTD cable (5) [for S Class only]. The motor is an interchangeable sub-assembly.



B) Temperature Probe (S Class only)

Function: Measure as well as possible the temperature of the piston-cylinder assembly.

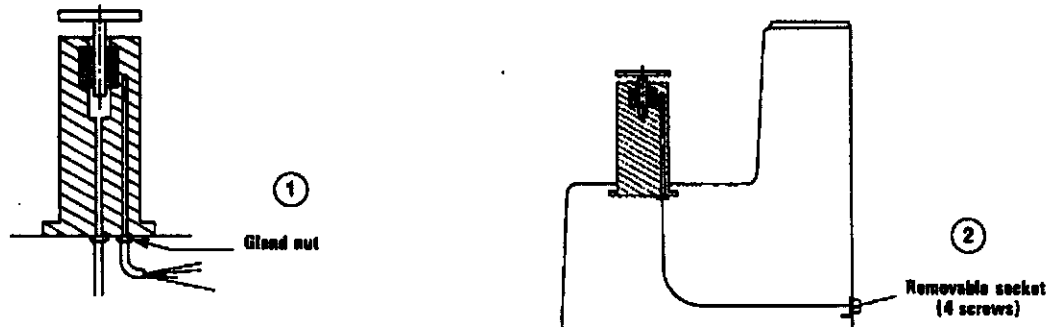
Description: Platinum RTD with 100 Ω nominal resistance at 0°C following DIN standard 43760. The 100 Ω value is given with an uncertainty of $\pm 0.01 \Omega$ which corresponds in temperature to $\pm 0.25^\circ\text{C}$. The DHI Laboratory determines the value of the resistance at 0°C inside the tolerance of the standard with an uncertainty of $\pm 0.02 \Omega$.

Serial number of the RTD



Installation of the Temperature Probe

The temperature probe is mounted in the mounting post as close as possible to the piston-cylinder. It makes possible valid and accurate temperature corrections. The probe is connected to a removable receptacle so that it can be removed and periodically recalibrated.



Removing The Probe

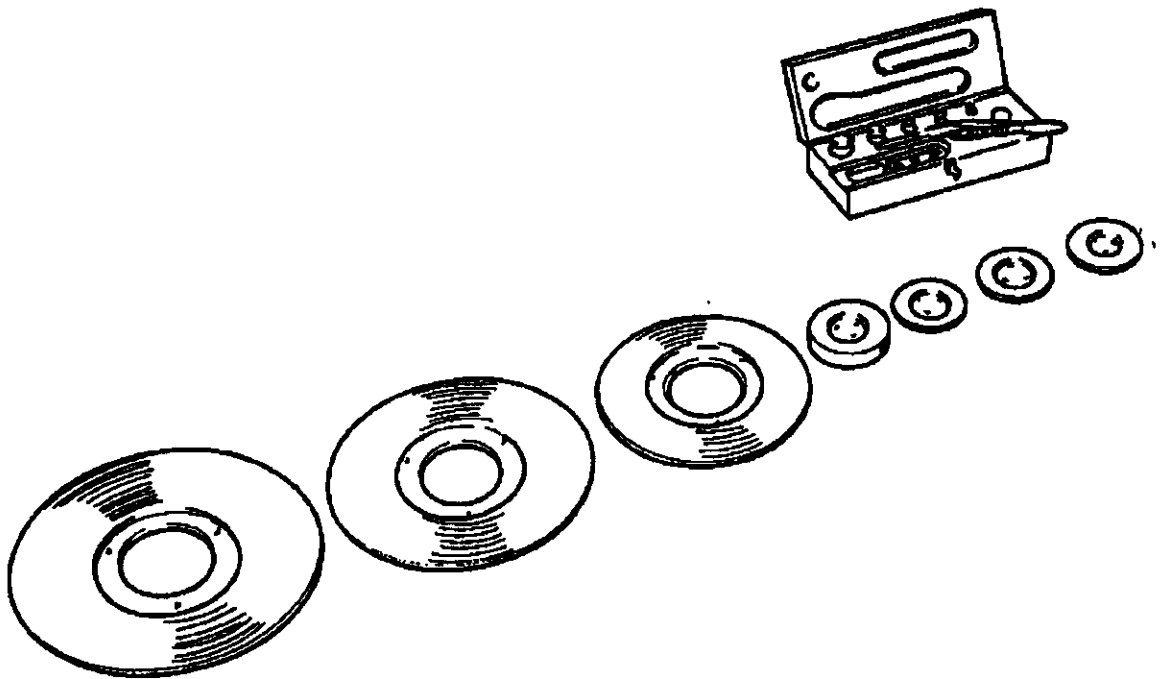
- Unscrew the gland (1) under the mounting post.
- Unscrew the 4 screws of the socket (2).
- Run the wire through the hole in the socket mount.
- Carefully remove the probe from the mounting post.



- **Mass Set**

Function: Define the value M which is subjected to acceleration due to gravity giving the force, F .

Description: Made of non-magnetic stainless steel. Masses of 1 kg and above are discs with a central hole to be slipped onto the mass carrying bell.



NOTE: Masses are engraved in kilograms which makes it possible to interchange piston-cylinders while using the same mass set.

- **Comparison Mass Set**

Function: Balancing the pressure under zero conditions.

Description: Same as above.

NOTE: Masses are deliberately under tared and bear no mass values engraved upon them. They have a different edge profile from the measuring masses.



(User Notes)



CHAPTER 3 - INSTALLATION AND START-UP

3.1 THE STANDARD AS DELIVERED

- The standard and its accessories are in a wooden cabinet.
- The four adjustable feet are retracted (screwed in).
- The visible level reservoirs are empty.
- Each mounting post has a stainless steel piston-cylinder plug installed, instead of the piston-cylinder.
- The masses are in their carrying cases.
- Each piston-cylinder is in its carrying case with the piston-cylinder key.

3.2 INSTALLING THE PISTON-CYLINDER

The overall piston-cylinder installation procedure includes the following:

- Setting the standard on a rigid table at a convenient height.
- Cleaning the piston-cylinders.
- Removing the piston-cylinder plugs.
- Installing the piston-cylinders.
- Filling the lubrication circuits.
- Purging the lubrication circuits.
- Purging the standard.

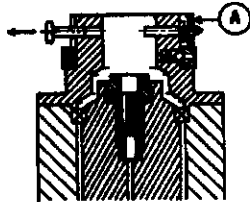
CLEANING THE PISTON-CYLINDER

Before installing the piston-cylinder, it must be cleaned with a liquid solvent.

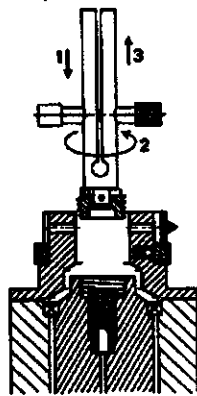
- Submerge the cylinder in the fluid and wipe the exterior and interior with a clean lint free cloth or tissue.
- Soak the piston in the fluid and wipe it off. NOTE: Care should be taken not to submerge the piston plate in the fluid.
- Put the piston in the cylinder. If both elements are properly cleaned, the piston moves freely without resistance in the cylinder.
- Once the elements are clean, lubricate the piston in the oil used in the standard and put the piston into the cylinder so that both pieces are lubricated.



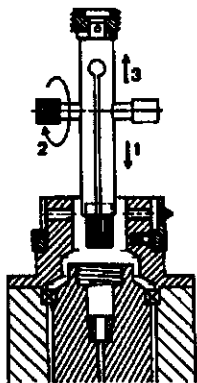
REMOVING THE PISTON-CYLINDER PLUG



- 1) Rotate ring (A) to expose the head of the piston travel limit pins. Remove each pin as it appears.



- 2) Insert the pin end of the piston-cylinder key into the cylinder retaining nut. Unscrew and remove the nut. (A spring-loaded ball keeps the nut on the key).

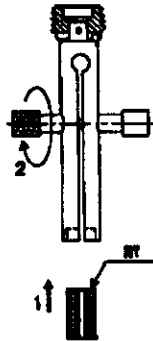


- 3) Invert the key and set the notched end over the plug and tighten the T handle as indicated. Remove the key and plug.



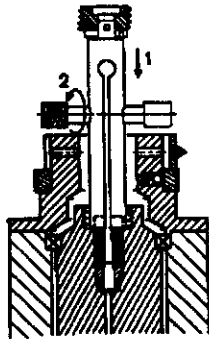
INSTALLING THE PISTON-CYLINDER

- Installing the Cylinder

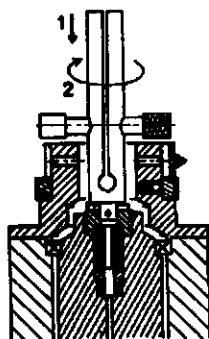


- 1) Put the cylinder into the notched end of the piston-cylinder key. Tighten T handle.

NOTE: The cylinder serial number and/or X notation must face upwards after installation. To do so, put this end of the cylinder into the key.



- 2) Insert the cylinder in the mounting post and loosen the T handle. Remove the key.

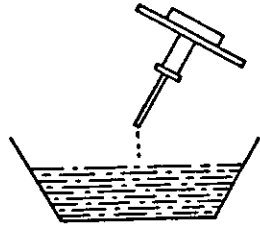


- 3) Invert tool. Reinstall the piston-cylinder retaining nut. Tighten to the end of its thread.

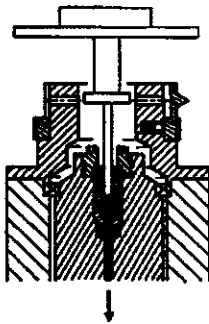
NOTE: Hand tighten only. High torque is not required.



- **Installing the Piston**

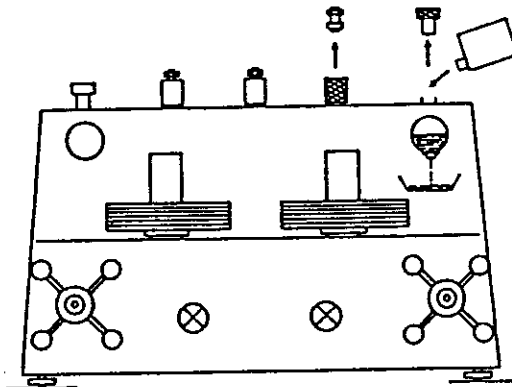


1) Dip the piston into the lubricant.



2) Insert the piston into the cylinder.

FILLING THE LUBRICATION CIRCUIT

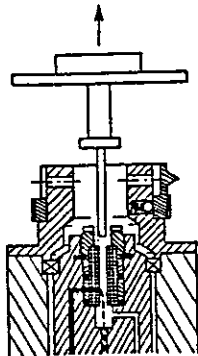


- 1) Remove the plug from the system under pressure connection.
- 2) Remove the visible level reservoir plug.
- 3) Slowly fill with fluid until fluid level is just above the pointer index in the window.
- 4) Repeat for the comparison side.

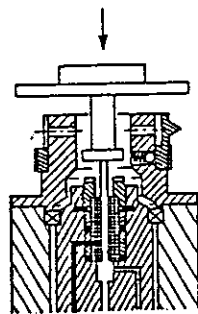


PURGING THE LUBRICATION CIRCUIT

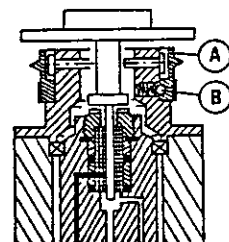
The lubrication circuit should be purged of any air which may be present.



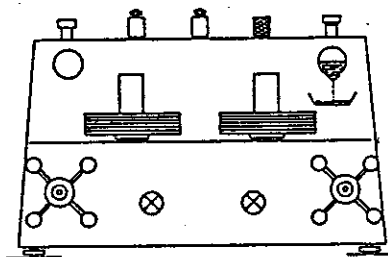
- 1) Remove the piston and watch for oil to run into the cylinder, or, for an observable level change in the visible level reservoir.



- 2) When liquid appears at the cylinder or level in the visible level reservoir has changed noticeably, re-insert piston in cylinder.



- 3) Replace the three piston travel limit pins.



- 4) If necessary, readjust fluid level in the visible level reservoir and reinstall plug. Then install system pressure connection plug.



PURGING THE STANDARD

Once the piston-cylinder has been installed, the standard must be purged of any lubricating fluid it may contain in the gas lines.

- 1) To drain standard:
 - unplug high and low pressure connecting heads
 - open sump drain cocks
 - allow circuit to drain
- 2) Verify that:
 - visible level reservoir plugs are tight
 - piston travel limit pins are in place
 - mass carrying bells are not on the pistons
 - plugs are secured in the quick-connecting heads
 - the inlet and exhaust valves are closed
 - sump drain cocks are closed
- 3) Connect a pneumatic supply to the system pressure connection.
- 4) Open the inlet valve to admit pneumatic pressure into the standard up to a pressure of about 150 psi (10 bar). Close the inlet valve.
- 5) Vent the pressure by loosening the drain cocks on the clarification chambers.
- 6) Repeat until no oil is discharged.

REMOVING A PISTON-CYLINDER

The standard must be at atmospheric pressure.

- 1) Remove the system pressure connection and the visible level reservoir plug.
- 2) Loosen the visible level reservoir drain cock and drain fluid into a cup.
- 3) Open sump drain cock.
- 4) Proceed in reverse order of piston-cylinder installation.



3.3 START-UP

The description below pertains to start-ups with the piston-cylinder already installed.

- 1) Level the standard using the 4 leveling feet and the bubble level:
 - Unscrew all four feet a few turns.
 - Screw in completely the front right foot.
 - Push down the left rear of the standard to stabilize it on the three feet that are screwed out.
 - Put the bubble into proper position on the right/left axis using the front left foot.
 - Put the bubble into the reference circle using the right rear foot.
 - Unscrew the front right foot to stabilize the standard.
- 2) If you have a standard with a switchable voltage motor, select the appropriate voltage (110V or 220V) with the switch on the inside of the standard.
- 3) Connect the power supply cable to the receptacle on the rear of the standard. Plug the cable into the power supply.
- 4) Connect the temperature probe cable to the receptacle on the rear of the standard and to a digital ohmmeter (S Class only).
- 5) Switch the motor on to rotate the piston.
- 6) Place the mass carrying bell on the piston plate and load four 2 kg masses on the bell.
- 7) Slowly admit pressure to the system until the piston rises.
- 8) Wait approximately two minutes. The purpose of this step is to assure proper seating of internal elements and to check the system for leaks. Close the gas inlet valve.
- 9) Unscrew the variable volume until the piston reaches its fully down position.
- 10) Vent pressure to return the system pressure back to atmospheric.

3.4 CALIBRATIONS: ELEVATED STATIC PRESSURE

- 1) Connect the system under test to the differential pressure standard.
- 2) With the exhaust valve open, screw out the two variable volumes.
- 3) Calculate the mass value required to balance the static pressure (P).
- 4) Load this mass onto the measuring piston.
- 5) Load an equivalent mass onto the comparison piston.
- 6) Open the high and low pressure isolation valves.
- 7) Close the gas exhaust valve.
- 8) Crack the gas inlet valve and raise the pressure until both pistons rise off their bottom stops.
- 9) Using the fractional weights provided, adjust the mass on the comparison piston so that both pistons are in equilibrium with their position indicator needles in the mid-position.



- 10) Close the low pressure isolation valve.
- 11) Calculate the mass value required for the first differential pressure increment and add this to the measuring piston.
- 12) Using the variable volumes, adjust the pressure on both sides so that the position indicating needles are again in the mid-position. The differential pressure increment is now defined.
- 13) Repeat Steps 11 and 12 for each pressure increment.
- 14) By reversing these procedures and calibrating against a falling differential pressure, the hysteresis characteristics of the instrument under test can be determined.

3.5 CALIBRATIONS: STATIC PRESSURE

- 1) Connect the instrument to the high pressure side of the Model 5500.
- 2) Open the gas exhaust valve and screw out the variable volume over 3/4's of its stroke.
- 3) Close the gas exhaust valve.
- 4) Calculate the quantity of mass required to balance the first static pressure value.
- 5) Load this mass value onto the measuring piston.
- 6) Close the low pressure isolation valve.
- 7) Open the high pressure isolation valve.
- 8) Crack the gas inlet valve to slowly increase the pressure until the piston lifts off its bottom stop.
- 9) The gas pressure will fall due to thermal effects.
- 10) Use the variable volume to adjust the gas pressure so the piston is floating in its mid-position.
- 11) Note the response of the instrument under test.
- 12) Calculate the quantity of mass required for the next pressure increment.
- 13) Repeat Steps 8 through 11 for each increment.
- 14) By reversing these procedures and calibrating against a falling pressure, the hysteresis characteristics of the instrument under test can be determined.

3.6 PARTICULARITIES OF PNEUMATIC OPERATION

Rapid variations of pneumatic pressure create significant changes in the temperature inside the standard. When added to the expansion and contraction of the internal elements of the standard, the result is that several minutes may be required to find stability after a pressure change.



3.7 PRECAUTIONS TO BE TAKEN TO ASSURE GOOD MEASUREMENTS

- 1) Clean the piston-cylinder thoroughly before installation.
- 2) Install the cylinder in the correct direction: serial number and/or X upwards.
- 3) Verify that the piston travel limit pins are installed.
- 4) Check that the fluid level in visible level reservoir is full.
- 5) Tighten the visible level reservoir cap while taking measurements.
- 6) Purge air from the standard and the system under test.
- 7) Level the standard and check the level when different mass values are loaded.
- 8) Check the power supply voltage.
- 9) Check that the piston is rotating.
- 10) Always put the piston in its fully down position before venting pressure.
- 11) Calibrate instruments in their normal operating position.
- 12) Check entire system for leaks.

3.8 SHUT-DOWN PROCEDURE

- 1) Close the gas cock of the pressure source.
- 2) Vent system to atmospheric pressure by opening the exhaust valve.
- 3) Open the inlet valve.
- 4) Screw in the variable volume.
- 5) Turn off the motor.
- 6) Put the masses in their storage cases.
- 7) Cover the standard with its plastic cover.

3.9 PERIODIC MAINTENANCE

- 1) Empty the oil from the oil run-off cup (NEVER REUSE THIS OIL).
- 2) Purge the system at the sump drain-cock.



3.10 PERIODIC OPERATIONAL CHECK

For regular use, it is recommended to return the standard to DHI every three years for a system overhaul. Production and high volume applications may require more frequent maintenance.

3.11 RECALIBRATION OF PISTON-CYLINDER AND MASSES

Periodic recalibration of the piston-cylinder and masses assures the long term reliability and optimal metrological performance of the system. Though other organizations can perform these calibrations, it is recommended that the DHI Calibration, Test and Service Division be used in order to receive data which allows the exploitation of piston K_n factors and whole number masses. The DHI calibration chain also documents long term repeatability of the system well inside of accuracy tolerances.

- **N Class Standards** - Two years after delivery, a complete recalibration by the CTS Division is advised. If no significant change from original data has occurred, adoption of a three year calibration cycle is recommended.
- **S, S' and S² Class Standards** - The first and second year after delivery, a complete recalibration by the CTS Division is advised. If no significant change from original data has occurred, adoption of a two year calibration cycle is recommended.

3.12 MOVING THE STANDARD

When moving the standard, complete the following:

- 1) Remove the piston-cylinder.
- 2) Store the piston and cylinder in their case.
- 3) Install the piston-cylinder plug into the mounting post.
- 4) Tighten the oil reservoir cap.
- 5) Plug the quick-connecting head.



3.13 SHIPPING THE STANDARD

When shipping the standard, the special shipping crates provided should be used.

- 1) Follow moving the standard instructions Steps 1 through 5 under Section 3.12.
- 2) Completely screw in the four adjustable feet.
- 3) Put the standard, the piston-cylinder, and the masses in their carrying cases.
- 4) Store the standard's accessories in the top of the standard's case.
- 5) Pack all the cases in their shipping crates.

3.14 STORING THE STANDARD

Follow the instructions given under Section 3.13 - Shipping the Standard. Storage temperature: -15°C $+65^{\circ}\text{C}$ ($+5$ to $+150^{\circ}\text{F}$).



(User Notes)



CHAPTER 4 - METROLOGICAL THEORY OF THE PRESSURE STANDARD

4.1 FUNDAMENTAL THEORY

The formula which gives the pressure at the reference level of the standard is:

$$P = \frac{Mg \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(\theta)}}$$

Where:

P :	pressure
M :	total mass on the piston
g :	acceleration due to gravity
ρ_a :	air density
ρ_m :	mass density
$A_{(\theta)}$:	effective area of the piston cylinder at temperature θ

The expression $\left(1 - \frac{\rho_a}{\rho_m}\right)$ is the correction due to the effect of air buoyancy on the masses. Under standard gravity and air density conditions, pressure is defined as:

$$P = \frac{M gn \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(\theta)}}$$

Where:

gn :	9.80665 m/s ² (standard gravity)
ρ_a :	air density at 20°C and atmospheric pressure of 1013.25 mbar: 1.2 kg/m ³
ρ_m :	density of stainless steel: 7920 kg/m ³
$A_{(\theta)}$:	effective area of the piston cylinder at temperature θ

In writing:

$$K_{N(\theta)} = \frac{gn \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(\theta)}} \quad \text{Eq. 1}$$

One obtains:

$$P = K_{N(\theta)} \times M \quad \text{Eq. 2}$$



The effective areas of DH piston-cylinders is such that K_N is a whole number when $\theta = 20^\circ\text{C}$.

$K_{N(20)}$ is called the normal conversion coefficient. It is a whole number for each piston-cylinder such that under standard conditions a mass of 1 kg is put into equilibrium by a pressure of $K_{N(20)}$ psi or $K_{N(20)}$ bar.

Piston-cylinders, for this model, are available with the following $K_{N(20)}$:

Measurements in psi

$$\begin{aligned} K_{N(20)} &= 20 \text{ psi/kg} \\ K_{N(20)} &= 50 \text{ psi/kg} \\ K_{N(20)} &= 100 \text{ psi/kg} \end{aligned}$$

Measurements in bar

$$\begin{aligned} K_{N(20)} &= 1.0 \text{ MPa/kg} \\ K_{N(20)} &= 2.0 \text{ MPa/kg} \\ K_{N(20)} &= 5.0 \text{ MPa/kg} \end{aligned}$$

CORRECTION FOR ACCELERATION DUE TO GRAVITY

At the location where the standard is used, the local gravity, gl , is usually different from standard gravity, gn . This gives:

$$P = \frac{M gl \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(\theta)}}$$

By writing:

$$K_{L(\theta)} = \frac{gl \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(\theta)}} \quad \text{Eq. 3}$$

From which:

$$K_{L(20)} = \frac{gl \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(20)}}$$

One can write:

$$K_{L(20)} = \frac{gl \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(20)}} = \frac{gn \left(1 - \frac{\rho_a}{\rho_m}\right)}{A_{(20)}} \times \frac{gl}{gn} = K_{N(20)} \frac{gl}{gn} \quad \text{Eq. 3'}$$

With:

$$C_g = \frac{gl}{gn}$$

C_g is the gravity correction. This value can be found in the C_g annex.



$K_{L(20)}$ is called the local conversion coefficient, which is defined by the piston-cylinder used and the location of use. For a given location K_L is a constant:

$$K_{L(20)} = K_{N(20)} \times C_g \quad \text{Eq. 4}$$

CORRECTION OF EFFECTIVE AREA AS A FUNCTION OF TEMPERATURE

When the temperature is other than 20°C, the change in effective area is defined by the following formula:

$$A_{(\theta)} = A_{(20)} [1 + (\alpha_c + \alpha_p) (\theta - 20)] \quad \text{Eq. 5}$$

Where:

$A_{(\theta)}$:	effective area of the piston cylinder at temperature θ
$A_{(20)}$:	effective area of the piston cylinder at temperature 20°C
α_c :	thermal expansivity of the cylinder
α_p :	thermal expansivity of the piston
θ :	temperature

GENERAL FORMULA

From Equations 3, 3', and 5, one obtains:

$$K_{L(\theta)} = K_{L(20)} [1 - (\alpha_p + \alpha_c) (\theta - 20)]$$

If

$$C_\theta = 1 - (\alpha_p + \alpha_c) (\theta - 20)$$

then

$$K_{L(\theta)} = K_{L(20)} \times C_\theta \quad \text{Eq. 6}$$

C_θ is the correction coefficient for temperature. This value can be found in the annex. Using Equations 6 and 4, it is possible to calculate P .

$$K_{L(20)} = K_{N(20)} \times C_g$$

$$P = K_{N(20)} \times C_g \times C_\theta \times M$$

AIR HEAD CORRECTION

The calculations on the previous page define the pressure at the bottom of the piston. The position of the bottom of the piston, when the piston is in mid-float position, is identified by a label "reference level" on the standard's housing.

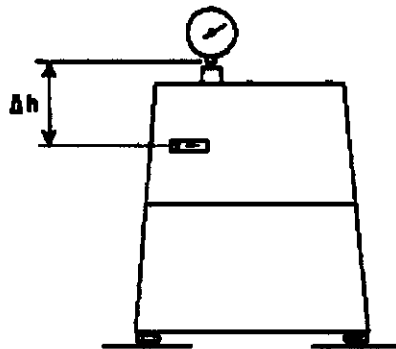


Generally, the instrument under test is not at the same height as the standard's reference level. Therefore, a correction defined by the following formula must be made:

$$\Delta P = \rho \times g \times \Delta h$$

Where:

ΔP :	fluid head correction.
ρ :	density of the fluid at operating pressure P
Δh :	difference in height between the reference levels of the standard and the instrument under test.
g :	acceleration due to gravity



The ΔP correction is negative if the instrument under test is above the standard's reference level:

$$P_{\text{instrument under test}} = P_{\text{standard}} - \Delta P$$

The ΔP correction is positive if the instrument under test is beneath the standard's reference level:

$$P_{\text{instrument under test}} = P_{\text{standard}} + \Delta P$$

NOTES:

- 1) Do not confuse use of ΔP here with differential pressure.
- 2) If ΔP transducer/transmitter is level, then gas head will be identical on both sides and no head correction is needed.



4.2 PRESSURE CALCULATION

The following parameters are given with the standard's calibration certificate:

$A(mes)$	Measured effective area at 20°C
$K_{N(20)}$	Normal conversion coefficient at 20°C
α_p	Thermal expansivity of the piston
α_c	Thermal expansivity of the cylinder
R_o	Resistance value of the RTD at 0°C

CALCULATION OF THE LOCAL CONVERSION COEFFICIENT AT 20°C

$$K_{L(20)} = K_{N(20)} \times C_g$$

C_g	correction coefficient for gravity for a given location
$K_{L(20)}$	is a constant for one location

CALCULATION OF THE PRESSURE AT THE REFERENCE LEVEL OF THE STANDARD

$$P = K_{L(0)} \times M$$

Where

$$K_{L(0)} = K_{L(20)} \times C_b$$

M : total mass on the piston

CALCULATION OF THE PRESSURE AT THE HEIGHT OF THE INSTRUMENT UNDER TEST

$$P_{\text{instrument under test}} = P_{\text{standard}} + \Delta P$$

ΔP is the fluid head correction which can be positive or negative.

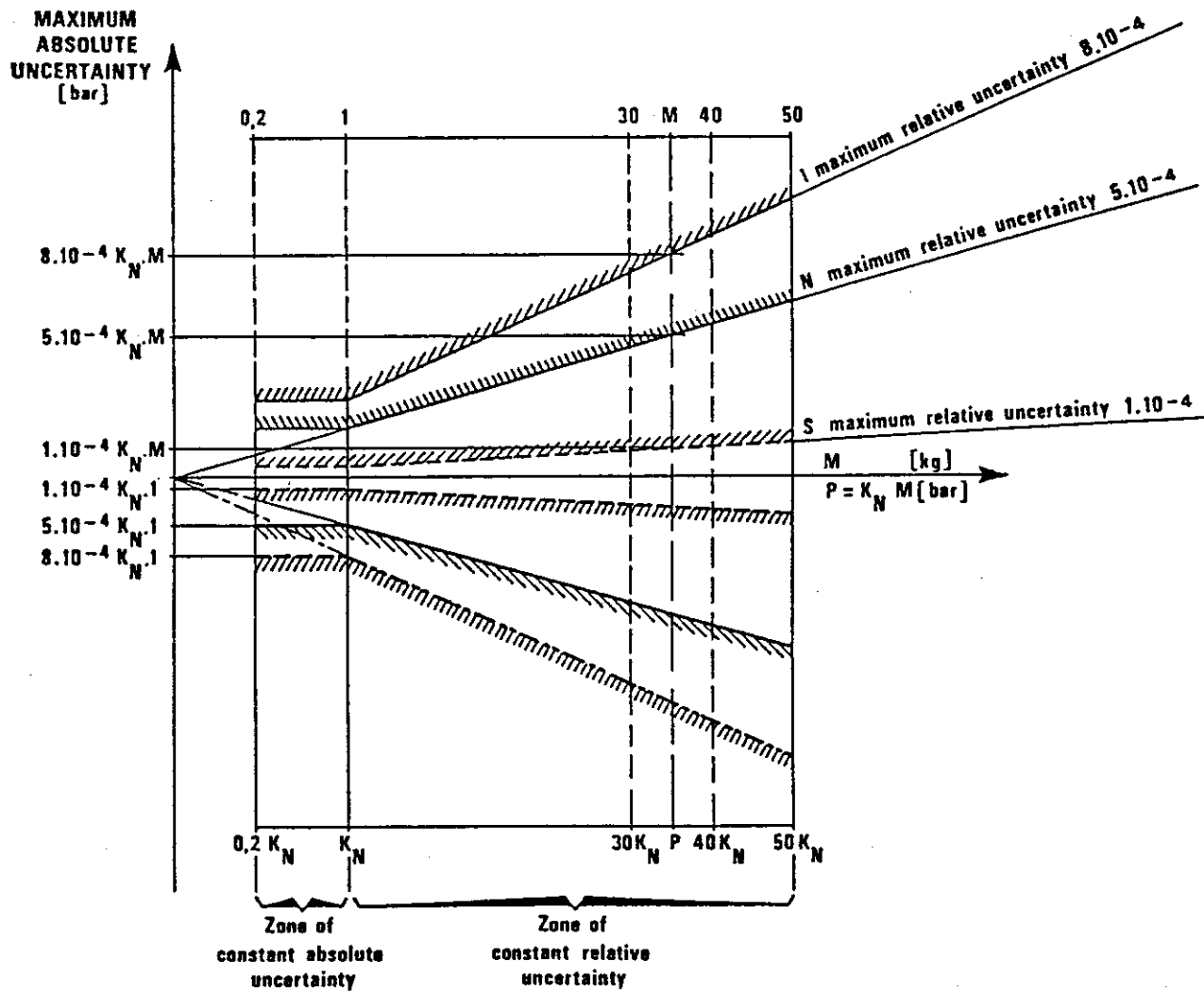
4.3 ACCURACY OF THE PRESSURE STANDARDS

The accuracy class of a pressure standard defines the relative uncertainty on a measured pressure. The lower limit is the pressure which puts into equilibrium 1 kg of mass, which is a value equal to the K_N of the piston-cylinder used. 1 kg is defined by the mass of the piston plus the mass of the mass carrying bell.

At 1 kg and above, there is enough rotational inertia to assure good mobility of the piston. In addition, the piston displacement indicator can be used.



Reference pressures between 0.2 kg (the piston alone) and 1 kg (piston + bell) can be defined. In this range, however, there is a constant absolute error equal to the relative error on the pressure defined by 1 kg.



4.4 TEMPERATURE PROBE (S, S' and S² accuracy only)

MEASURING PRINCIPAL

In the range of 0 - 40°C, the temperature is proportional to the change in resistance of the platinum RTD following the formula:

$$\theta = \frac{R_{\theta} - R_0}{0.389}$$

Where:

θ :	temperature in °C
R_{θ} :	read resistance of the platinum RTD at temperature θ
R_0 :	resistance of the platinum RTD at 0°C (supplied by DHI)
0.389:	conversion coefficient of Ω to °C following DIN norm 43760

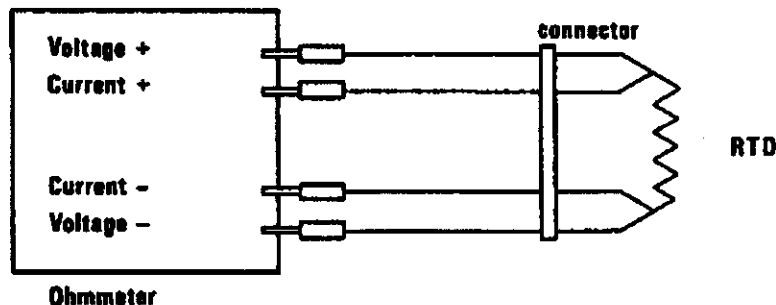
The resistance used must be the resistance of the platinum RTD only excluding the resistance of the read-out cable. This is why a 4-wire cable is used.

- Two wires are used to give a constant power supply to the RTD (5 mA max).
- Two wires are used to measure the resistance of the RTD.

MEASUREMENTS

Use an ohmmeter allowing 4-wire measurements. In this case, there is a direct read-out of the R value.

- **Connecting the temperature probe**
 - Connect the read-out cable to the receptacle on the back of the standard.
 - Connect the 4 plugs of the cable to a digital ohmmeter (supply current must not exceed 5mA).



- The ohmmeter should be calibrated to read a value of about 100 Ω with an accuracy of $\pm 0.01 \Omega$.



Example of a calculation

Value read on the ohmmeter: 107.32 Ω
 Ohmic resistance at 0°C: 99.98 Ω

$$\theta = \frac{107.32 - 99.98}{0.389} = 18.87^{\circ}\text{C}$$

Using an ohmmeter allowing only 2-wire measurements. The resistance measured is the resistance of the connecting leads. To diminish the effect of the resistance of the connecting leads, leads R_1 and R_2 and leads R_3 and R_4 should be connected in parallel.

R_1 red plug	---	same end of the RTD
R_2 red plug	---	
R_3 blue plug	---	same end of the RTD
R_4 blue plug	---	

Since the length of the leads is approximately equal, we can say:

$$R_1 \cong R_2 \cong R_3 \cong R_4$$

When the leads are in parallel, the effect of the resistance of the leads in the measurement is:

$$\frac{R_1 + R_2}{4} \text{ for leads } R_1 \text{ and } R_2$$

$$\frac{R_3 + R_4}{4} \text{ for leads } R_3 \text{ and } R_4$$

given:

$$\frac{R_1 + R_2}{4} + \frac{R_3 + R_4}{4}$$

Therefore, from the value measured in 2 leads, the value:

$$\frac{R_1 + R_2 + R_3 + R_4}{4}$$

must be subtracted to obtain the value of the resistance of the RTD.

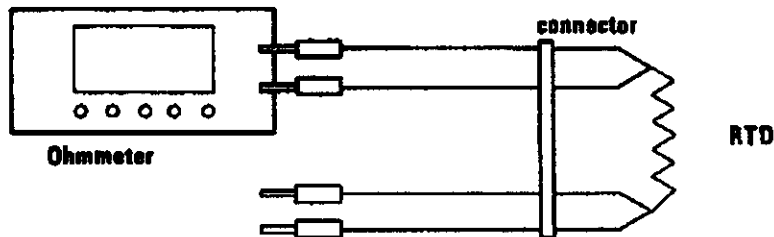
• **Determination Of The $R_1 + R_2$ Resistance Value (Red Plugs)**

- Put the ohmmeter in measuring mode.
- Connect the temperature probe cable to the receptacle on the standard.
- Measure the resistance between the two red leads.
- Read the value (about 0.3 Ω).



- **Determination Of The $R_1 + R_2$ Resistance Value (Blue Plugs)**

Proceed as for $R_1 + R_2$ on previous page using the blue plugs rather than the red plugs. Resistance should be about 0.3Ω .



- **Measuring The Resistance Of The RTD To Determine The Temperature**

- Parallel the two red plugs by plugging one into the other.
- Parallel the two blue plugs by plugging one into the other.
- Connect the red plugs and blue plugs to the ohmmeter (take care that there is no contact between the red and blue plugs).
- Read the resistance value (about 107Ω)

$$R = R_0 - \left(\frac{R_1 + R_2}{4} + \frac{R_3 + R_4}{4} \right)$$

- **Temperature Calculation**

$$R_0 = R - \left(\frac{R_1 + R_2}{4} + \frac{R_3 + R_4}{4} \right)$$

$$\theta = \frac{R_0 - R_0}{0.389}$$

- **Example Of Temperature Calculation**

Measure: $R_1 + R_2 = 0.3$
 $R_3 + R_4 = 0.4$

$$R_0 - \left(\frac{R_1 + R_2}{4} \right) + \left(\frac{R_3 + R_4}{4} \right) = 107.5 \Omega$$

from which:

$$R_0 = 107.5 \Omega - \left(\frac{R_1 + R_2}{4} + \frac{R_3 + R_4}{4} \right)$$

$$R_0 = 107.5 \Omega - \left(\frac{0.3}{4} + \frac{0.4}{4} \right)$$



$$R_0 = 107.5 - (0.08 + 0.1)$$

$$R_0 = 107.5 - 0.18$$

$$R_0 = 107.32 \Omega$$

For ohmic resistance of the RTD at 0°C of 99.98 (value furnished by DHI given on a stamped label on the back of the standard and in the Standard's Technical Data) the temperature is:

$$\theta = \frac{R_0 - R_0}{0.389} = \frac{107.32 - 99.98}{0.389} = 18.87^\circ\text{C}$$

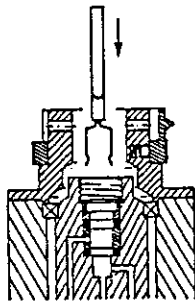
• **Remark**

- For a given RTD cable used with a given standard, the values of $R_1 + R_2$ and $R_3 + R_4$ are constants.
- Using a different cable on the same standard or vice-versa, changes the values of $R_1 + R_2$ and $R_3 + R_4$.
- The temperature value obtained using this method is accurate to $\pm 1^\circ\text{C}$ which corresponds to $\pm 0.001\%$ on the effective area of the piston.

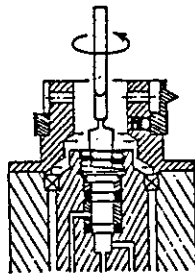


CHAPTER 5 - MAINTENANCE

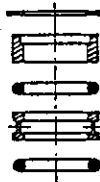
5.1 CHANGING THE MOUNTING POST O-RING ASSEMBLY



- 1) Remove the cylinder and insert the special tool into the notches in the circlip.



- 2) Remove the circlip by rotating the tool.

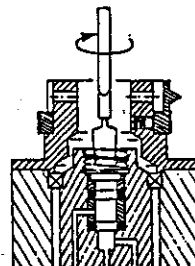


- 3) Remove the first spacer, the first O-ring, the second spacer and the second O-ring. Replace the O-rings and reassemble.

NOTE:

Arrange the O-rings and spacers as shown.

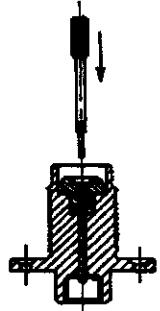
Circlip	p/n- 36866
Spacer	p/n- 30188
O-ring	p/n- R-13
Spacer	p/n- 30187
O-ring	p/n- R-13



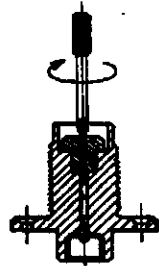
- 4) Reinstall the circlip to the bottom of the thread.



5.2 CHANGING THE QUICK-CONNECTING HEAD O-RING ASSEMBLY

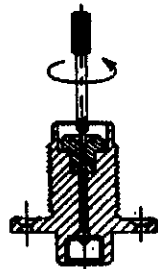


- 1) Remove the knurled nut from the quick-connecting head.



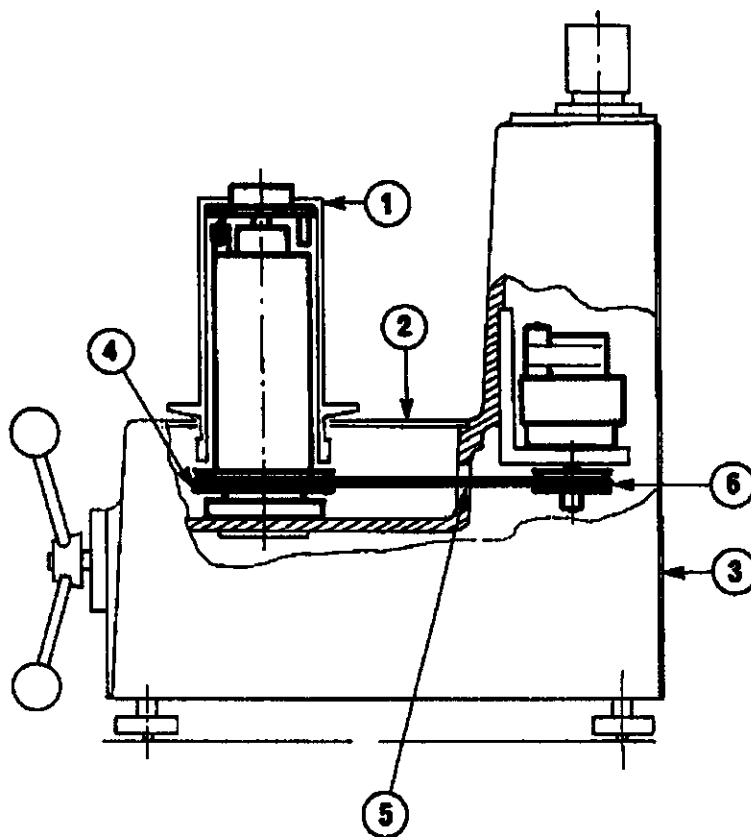
- 2) Screw the special tool into the O-ring assembly and pull upwards to remove the O-ring assembly.

Upper O-ring	p/n- R2
O-ring assembly	p/n- 41087
Anti-extrusion ring	p/n- 40900
Lower O-ring	p/n- R5



- 3) Screw a new O-ring assembly onto the special tool, push it into quick-connecting head. Unscrew and remove the special tool.



5.3 REPLACING THE DRIVE BELT

- 1) Remove the mass carrying bell (1), the upper cover (2) and the rear cover (3).
- 2) Remove the used belt.
- 3) Slip the new belt over the pulley (4) and position it in the groove. Pass the belt through the opening (5) and position it in the groove of the motor pulley (6).
- 4) Reinstall the protective covers, (2) and (3).



(User Notes)



CHAPTER 6 - TROUBLESHOOTING

<u>SYMPTOM</u>	<u>POSSIBLE CAUSE</u>	<u>SOLUTION</u>
• Poor piston mobility	• Dirty piston-cylinder	• Remove and clean the piston-cylinder (see Section 3.2).
• Piston does not rotate	• Bad connection of the motor power supply cable	• Check motor cable.
	• Blown fuse	• Replace fuse (see Section 2.3).
	• Slip or deterioration of the drive belt	• Reinstall or replace drive belt (see Section 5.3).
	• Burned out motor	• Replace electrical assembly (see Section 2.3).
• Aberrant measurements	• Air introduced into fluid	• Purge air from lubrication system.
	• Impure fluids	• Purge spent oil from standard.
• Poor pressure stability	• Leak in hydraulic circuit	
	Standard not leaking-	• Check test circuit.
	Standard is leaking- Visible	• Tighten sump drain cock.
		• Replace connecting head O-ring assembly.
		• Change the measuring post O-ring assembly.
		• Tighten gland nut in hydraulic circuit.
		• Replace the outlet check valve.
	Not visible	• Replace inlet valve if piston rises when system pressure is less than supply pressure and falls when system pressure is greater than supply pressure.



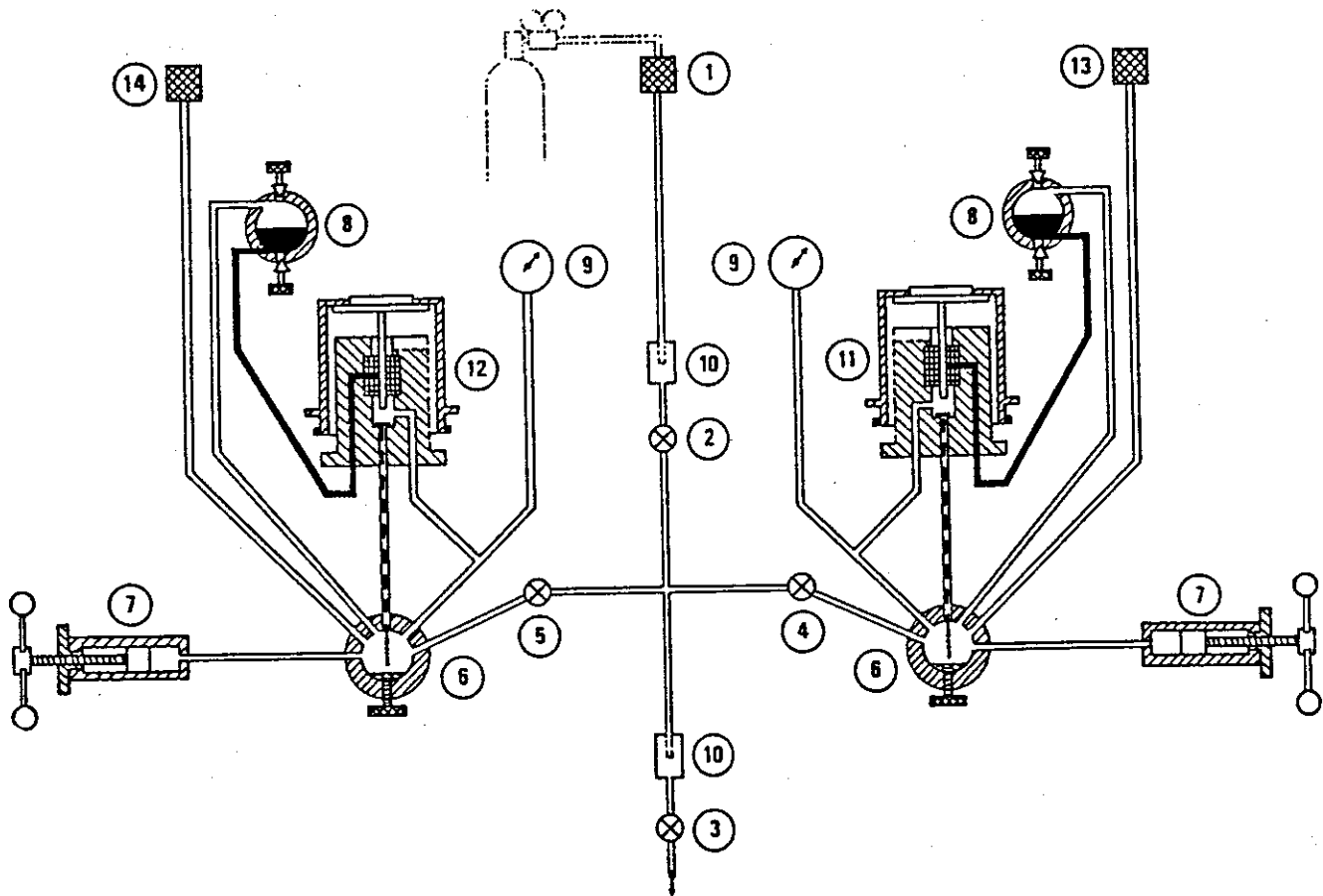
<u>SYMPTOM</u>	<u>POSSIBLE CAUSE</u>	<u>SOLUTION</u>
<ul style="list-style-type: none">• Poor pressure stability	<ul style="list-style-type: none">• Leak in hydraulic circuit Not visible continued-	<p>Change a variable volume if leak stops when one variable volume is isolated with a pressure plug on the pressure manifold.</p> <ul style="list-style-type: none">• Change gas inlet valve if problem persists with both HP and LP isolation valves open.• Close both isolation valves, change one that leaks.• Check external pipework for leaks.• Check valves for gas tightness.

NOTE: Part numbers for each subassembly are given in Section 2.2.



CHAPTER 7 - SCHEMATIC

HYDRAULIC CIRCUIT SCHEMATIC



- | | |
|----------------------------------|--------------------------------------|
| 1) Gas Pressure Inlet Connection | 8) Visible Level Lubricant Reservoir |
| 2) Inlet Valve | 9) Pressure Gauge |
| 3) Exhaust Valve | 10) Coarse Filter |
| 4) HP Isolation Valve | 11) Measuring Post (P + DP) |
| 5) LP Isolation Valve | 12) Comparison Post |
| 6) Pressure Manifold/sump | 13) HP Pressure Connection |
| 7) Variable Volume | 14) LP Pressure Connection |



(User Notes)



ANNEXES

- Values of the Correction Factor C_p
- Temperature Correction: Tungsten Carbide only
- Temperature Correction: Steel and Tungsten Carbide
- Pressure Conversion Factors
- DH 400 High Pressure Flexible Tubes
- Spinell Material Data Sheet



**VALUES OF THE CORRECTION FACTOR C_g
AS A FUNCTION
OF LOCAL GRAVITY**

$$C_g = \frac{g_L}{g_M}$$

g_L : local gravity

g_M : standard gravity = 9.80665 m/s²

g_L (m/s ²)	C_g
9.7800	0.99728
05	33
9.7810	0.99738
15	44
9.7820	0.99749
25	54
9.7830	0.99759
35	64
9.7840	0.99769
45	74
9.7850	0.99779
55	84
9.7860	0.99789
65	95
9.7870	0.99800
75	05
9.7880	0.99810
85	15
9.7890	0.99820
95	25
9.7900	0.99830
05	35
9.7910	0.99840
15	46
9.7920	0.99851
25	56

g_L (m/s ²)	C_g
9.7930	0.99861
35	66
9.7940	0.99871
45	76
9.7950	0.99881
55	86
9.7960	0.99891
65	96
9.7970	0.99902
75	07
9.7980	0.99912
85	17
9.7990	0.99922
95	27
9.8000	0.99932
05	37
9.8010	0.99942
15	47
9.8020	0.99953
25	58
9.8030	0.99963
35	68
9.8040	0.99973
45	78
9.8050	0.99983
55	88

g_L (m/s ²)	C_g
9.8060	0.99993
9.80665	1.00000
9.8070	1.00004
75	09
9.8080	1.00014
85	19
9.8090	1.00024
95	29
9.8100	1.00034
05	39
9.8110	1.00044
15	49
9.8120	1.00055
25	60
9.8130	1.00065
35	70
9.8140	1.00075
45	70
9.8150	1.00085
55	90
9.8160	1.00095
65	100
9.8170	1.00106
75	11
9.8180	1.00116
85	21

g_L (m/s ²)	C_g
9.8190	1.00126
95	31
9.8200	1.00136
05	41
9.8210	1.00146
15	51
9.8220	1.00157
25	62
9.8230	1.00167
35	72
9.8240	1.00177
45	82
9.8250	1.00187
55	92
9.8260	1.00197
65	202
9.8270	1.00208
75	13
9.8280	1.00218
85	23
9.8290	1.00228
95	33
9.8300	1.00238
05	43
9.8310	1.00248
15	53



TEMPERATURE CORRECTION**Piston And Cylinder In Tungsten Carbide**

$$\text{value of } C_{\theta} = 1 - (\alpha_p + \alpha_c)(\theta - 20) \quad \alpha_p + \alpha_c = 9 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$$

(°C)	C_{θ}
5	1.00014
6	1.00013
7	1.00012
8	1.00011
9	1.00010
10	1.00009
11	1.00008
12	1.00007
13	1.00006
14	1.00005
15	1.00004
16	1.00004
17	1.00003
18	1.00002
19	1.00001

(°C)	C_{θ}
20	1.00000
21	0.99999
22	0.99998
23	0.99997
24	0.99996
25	0.99996
26	0.99995
27	0.99994
28	0.99993
29	0.99992
30	0.99991
31	0.99990
32	0.99989
33	0.99988
34	0.99987

(°C)	C_{θ}
35	0.99986
36	0.99986
37	0.99985
38	0.99984
39	0.99983
40	0.99982
41	0.99981
42	0.99980
43	0.99979
44	0.99978
45	0.99978
46	0.99977
47	0.99976
48	0.99975
49	0.99974



TEMPERATURE CORRECTION

Piston In Steel And Cylinder In Tungsten Carbide

$$C_{\theta} = 1 - (\alpha_p + \alpha_c)(\theta - 20)$$

- α_p : Thermal expansivity of steel = $1.05 \times 10^{-5} [^{\circ}\text{C}^{-1}]$
- α_c : Thermal expansivity of tungsten carbide = $4.50 \times 10^{-6} [^{\circ}\text{C}^{-1}]$
- θ : Temperature of the piston cylinder [$^{\circ}\text{C}$]

($^{\circ}\text{C}$)	C_{θ}
5	1.00023
6	1.00021
7	1.00020
8	1.00018
9	1.00017
10	1.00015
11	1.00014
12	1.00012
13	1.00011
14	1.00009
15	1.00008
16	1.00006
17	1.00005
18	1.00003
19	1.00002

($^{\circ}\text{C}$)	C_{θ}
20	1.00000
21	0.99999
22	0.99997
23	0.99996
24	0.99994
25	0.99993
26	0.99991
27	0.99990
28	0.99988
29	0.99987
30	0.99985
31	0.99984
32	0.99982
33	0.99981
34	0.99979

($^{\circ}\text{C}$)	C_{θ}
35	0.99978
36	0.99976
37	0.99975
38	0.99973
39	0.99972
40	0.99970
41	0.99969
42	0.99967
43	0.99966
44	0.99964
45	0.99963
46	0.99961
47	0.99960
48	0.99958
49	0.99957



PRESSURE UNIT CONVERSIONS

	Pa (N/m ²)	bar	psi ⁽¹⁾	kg/cm ² ⁽¹⁾	mm Hg (torr) ⁽¹⁾⁽²⁾	in Hg ⁽¹⁾⁽²⁾	m H ₂ O ⁽¹⁾⁽³⁾	in H ₂ O ⁽¹⁾⁽³⁾
1 Pa (N/m ²) =	1	1.000000 x 10 ⁻⁵	1.450377 x 10 ⁻⁴	1.019716 x 10 ⁻⁵	7.500627 x 10 ⁻³	2.953003 x 10 ⁻⁴	1.019716 x 10 ⁻⁴	4.014613 x 10 ⁻³
1 bar =	1.000000 x 10 ⁵	1	1.450377 x 10	1.019716	7.500627 x 10 ²	2.953003 x 10	1.019716 x 10	4.014613 x 10 ²
⁽¹⁾ 1 psi =	6.894757 x 10 ³	6.894757 x 10 ⁻²	1	7.030696 x 10 ⁻²	5.171500 x 10	2.036024	7.030696 x 10 ⁻¹	2.767990 x 10
⁽¹⁾ 1 kg/cm² =	9.806650 x 10 ⁻⁴	9.806650 x 10 ⁻¹	1.422334 x 10	1	7.355602 x 10 ²	2.895906 x 10	1.000000 x 10	3.937008 x 10 ²
⁽¹⁾⁽²⁾ 1 mm Hg (torr) =	1.333222 x 10 ²	1.333222 x 10 ⁻³	1.933675 x 10 ²	1.359508 x 10 ⁻³	1	3.937008 x 10 ⁻²	1.359508 x 10 ⁻²	5.352394 x 10 ⁻¹
⁽¹⁾⁽²⁾ 1 in Hg =	3.386384 x 10 ³	3.386384 x 10 ⁻²	4.911534 x 10 ⁻¹	3.453150 x 10 ⁻²	2.540000 x 10	1	3.453150 x 10 ⁻¹	1.359508 x 10
⁽¹⁾⁽³⁾ 1 m H₂O =	9.806650 x 10 ³	9.806650 x 10 ⁻²	1.422334	1.000000 x 10 ⁻¹	7.355602 x 10	2.895906	1	3.937008 x 10
⁽¹⁾⁽³⁾ 1 in H₂O =	2.490889 x 10 ²	2.490899 x 10 ⁻³	3.612729 x 10 ⁻²	2.540000 x 10 ⁻³	1.868323	7.355602 x 10 ⁻²	2.540000 x 10 ⁻²	1

(1) Normal gravity:

$g_n = 9.80665 \text{ m/s}^2$

(2) Density of mercury at 0°C and standard atmospheric pressure (101325 Pa):

$\text{Hg} = 1.359508 \times 10^4 \text{ kg/m}^3$

(3) Density of water at 4°C and standard atmospheric pressure (101325 Pa):

$\text{H}_2\text{O} = 1.000000 \times 10^3 \text{ kg/m}^3$



(User Notes)

